

# Energy and Isospin Dependence of Elliptic Flow - An Alternative Analysis of the LAND-FOPI Data

Maja Zoric, Dr. Yvonne Leifels

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# Outline :

- Description of the experimental setup
- Available statistics
- Data analysis (n/H)
  - pt integrated  $v_2$
  - differential squeeze-out  $v_2(\text{pt})$
  - squeeze-out ratio
- Consistency checks, evaluation of systematic errors
- Conclusions and Prospects

# Relevant variables

- Normalised transverse momentum
- Q - vector

$$p_{t0} = p_{\perp,part}/p_{proj}$$

$$\vec{Q} = \sum_{\nu} w_{\nu} \vec{p}_t(\nu)$$

- Rapidity

$$y = 0.5 \ln \left( \frac{1 + \beta_z}{1 - \beta_z} \right)$$

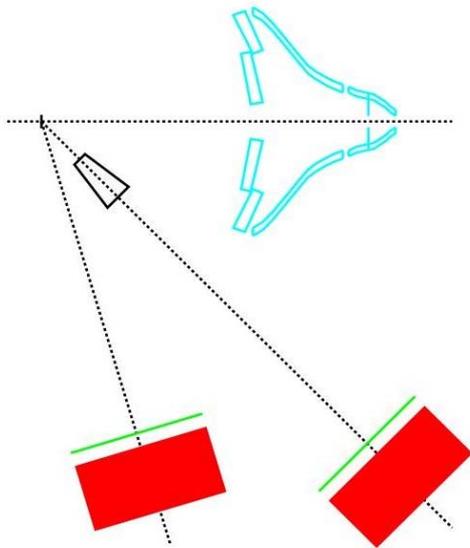
$$w_{\nu} = 1 \quad y > y_{cm}, \quad w_{\nu} = -1 \quad y < y_{cm}$$

- Normalised rapidity

$$y_0 = y_{part}/y_{proj}$$

$p_{proj}/\text{MeVc}^{-1}$	$Y_{proj}$	E/MeV
432	0.896	400
529	1.0815	600
610	1.2313	800

# Description of the experimental setup



LAND:

- Velocity vectors of neutrons and light charged particles
- Mass determination from total deposited energy

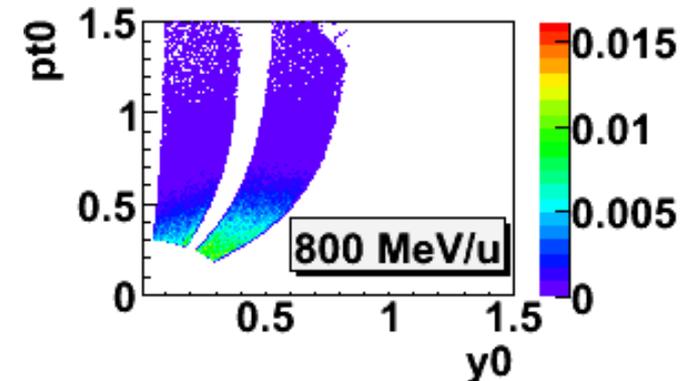
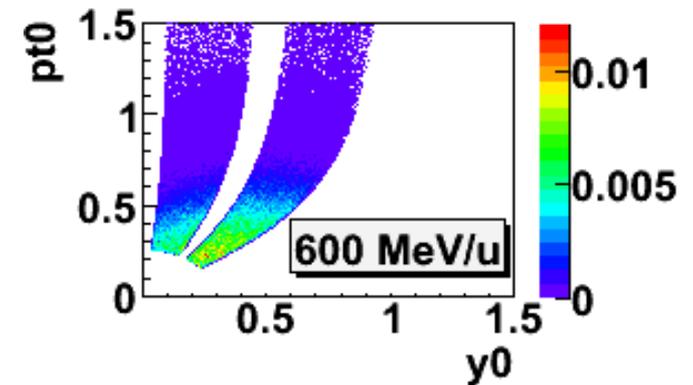
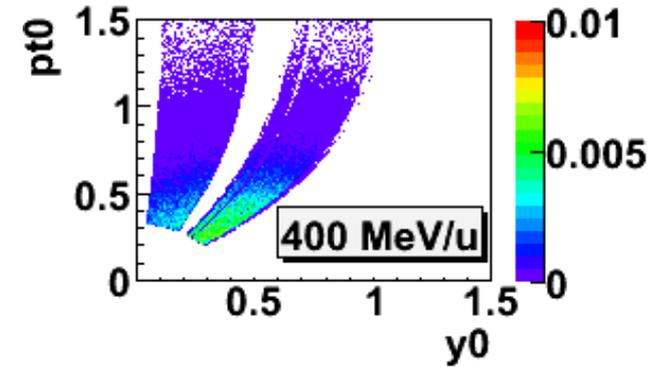
PLAWA:

- Charge from  $\Delta E$ -TOF
- Reaction plane determination from total transverse momentum of charged particles

LAND 1:  $\theta_{\text{lab}} = 45^\circ \pm 8^\circ$

PLAWA:  $1^\circ \leq \theta_{\text{lab}} \leq 30^\circ$

LAND 2:  $\theta_{\text{lab}} = 73^\circ \pm 12^\circ$



# Statistics overview

total evt. evt. cut particles part. cut n H ( × 10<sup>5</sup> )

400 MeV/u

<b>18.0</b>	<b>30 %</b>	<b>12.3</b>	<b>6.6</b>	<b>2.8</b>	<b>2.9</b>
<b>2.4</b>	<b>26 %</b>	<b>0.9</b>	<b>0.32</b>	<b>0.01</b>	<b>0.004</b>
<b>4.7</b>	<b>23 %</b>	<b>1.2</b>	<b>0.14</b>	<b>0.1</b>	<b>0.03</b>

no shadow bar  
shadow bar 1  
shadow bar 2

600 MeV/u

<b>23.4</b>	<b>40 %</b>	<b>28.3</b>	<b>18.9</b>	<b>8.6</b>	<b>8.8</b>
<b>8.7</b>	<b>40%</b>	<b>7.5</b>	<b>0.3</b>	<b>0.18</b>	<b>0.06</b>
<b>8.0</b>	<b>43 %</b>	<b>5.8</b>	<b>1.2</b>	<b>0.8</b>	<b>0.36</b>

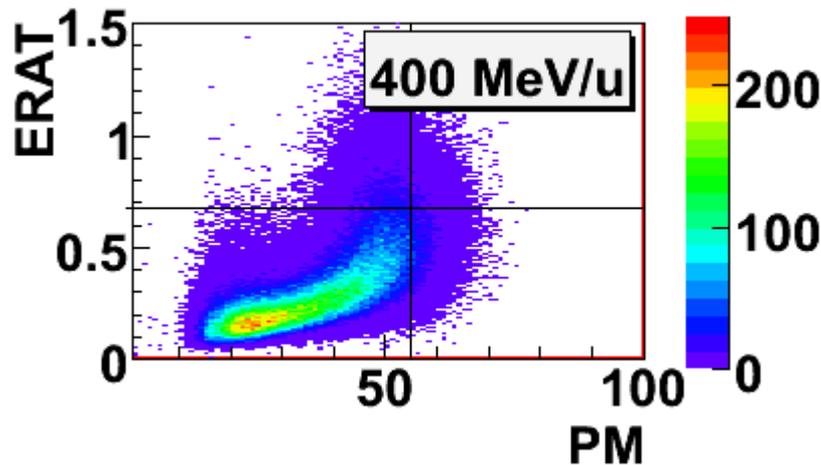
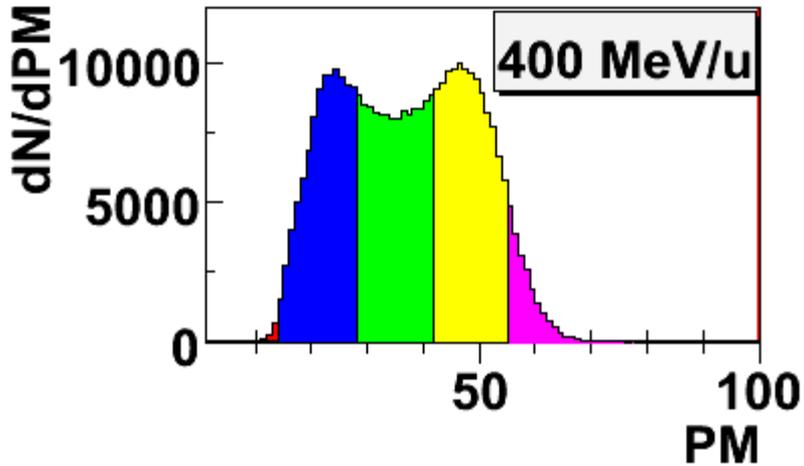
no shadow bar  
shadow bar 1  
shadow bar 2

800 MeV/u

<b>13.7</b>	<b>38 %</b>	<b>17.2</b>	<b>9.7</b>	<b>4.8</b>	<b>4.0</b>
<b>5.0</b>	<b>38 %</b>	<b>4.6</b>	<b>0.12</b>	<b>0.08</b>	<b>0.03</b>
<b>7.4</b>	<b>41 %</b>	<b>5.6</b>	<b>0.98</b>	<b>0.62</b>	<b>0.3</b>

no shadow bar  
shadow bar 1  
shadow bar 2

# Details of analysis procedure



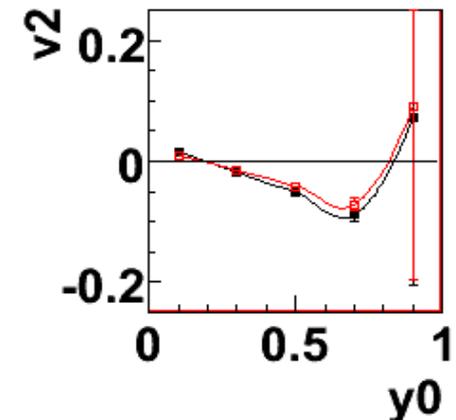
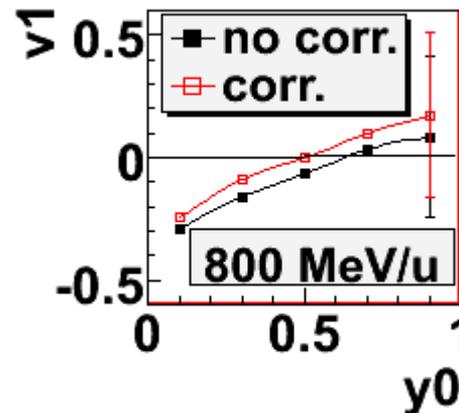
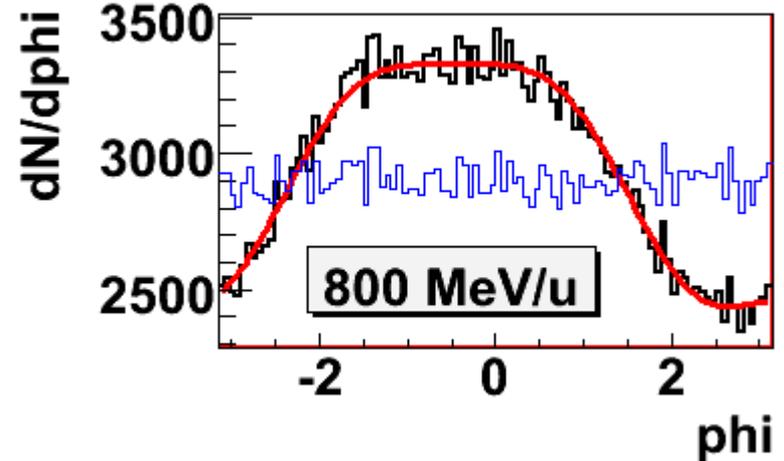
- 5 PLAWA multiplicity and 5 ERAT bins
- ERAT 5: Identical cross section for last bin of both observables

$$ERAT = \frac{\sum_{part.} E_{\perp}}{\sum_{part.} E_{\parallel}}$$

$$F(\Delta\phi) = N(1 + 2(v_1 \cos(\Delta\phi) + v_2 \cos(2\Delta\phi)))$$

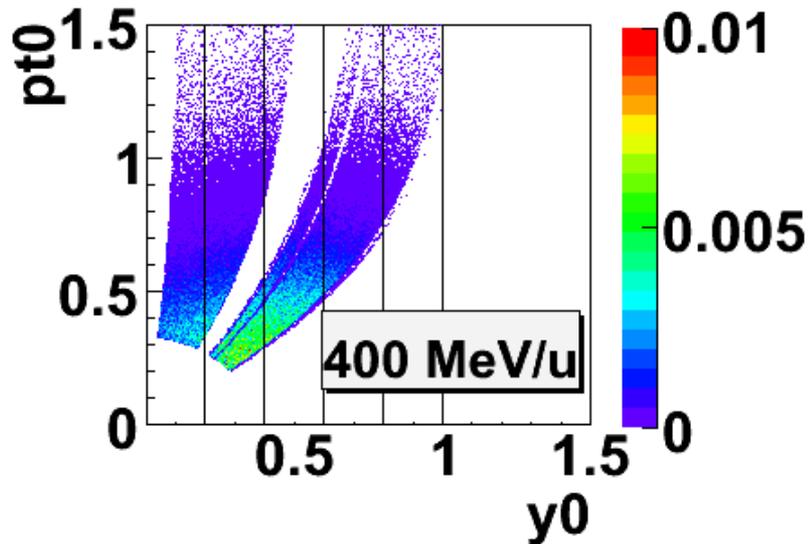
# Details of analysis procedure

- Correction on detector acceptance and efficiency included
- Substraction of normalised shadow bar run data
- Correction of anisotropic asymuthal distribution of reaction plane after applied trigger cuts
- Corrected weights calculated for each shadow/ non shadow bar run data

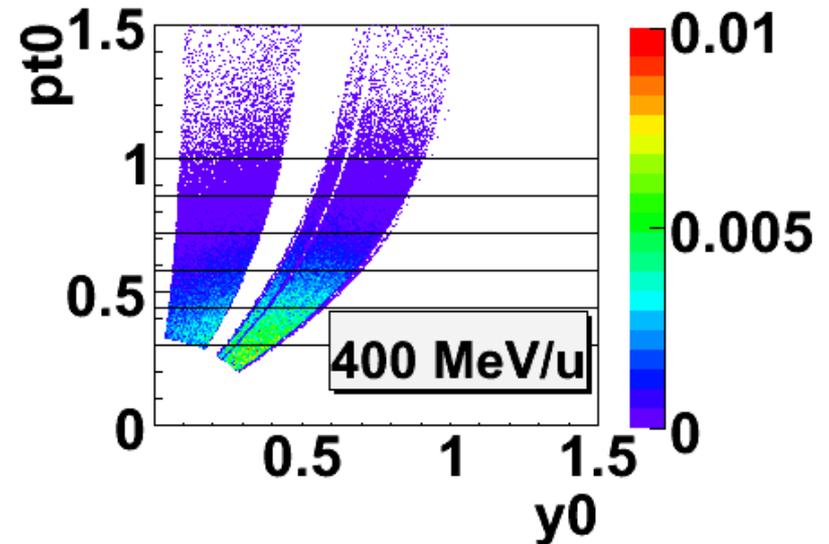


# Details of analysis

pt integrated flow:



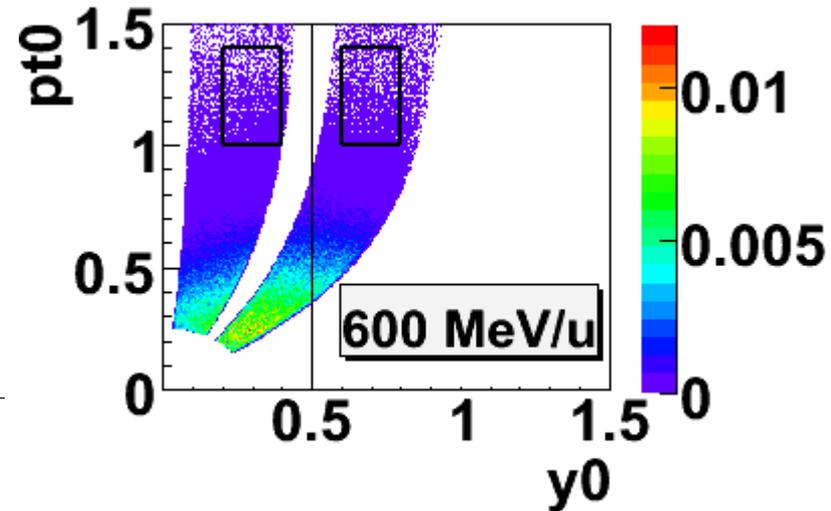
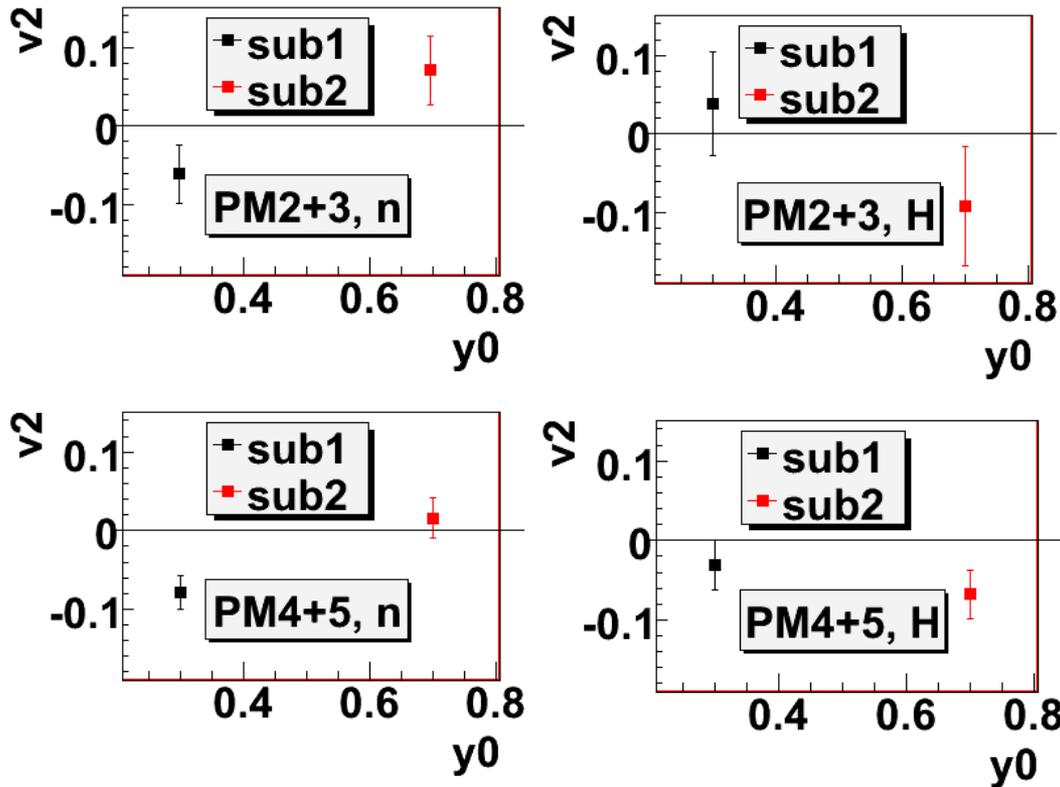
differential flow:



- 5 equidistant bins in normalised rapidity and transverse momentum

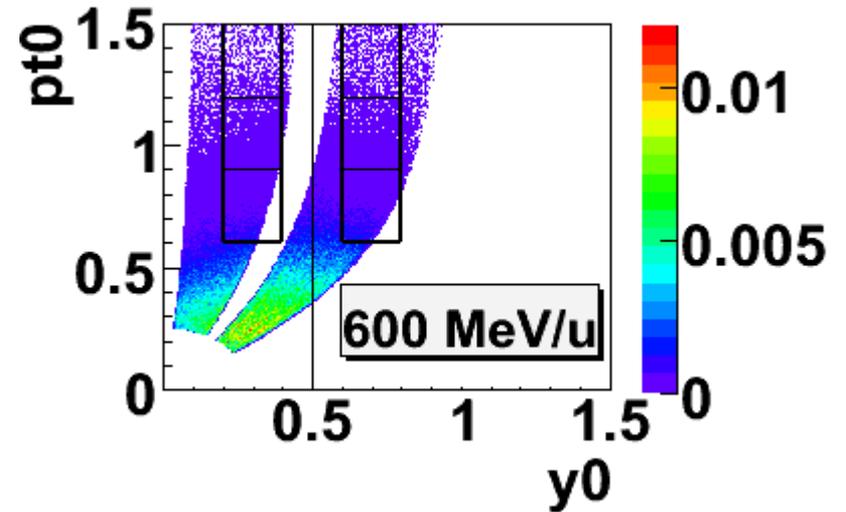
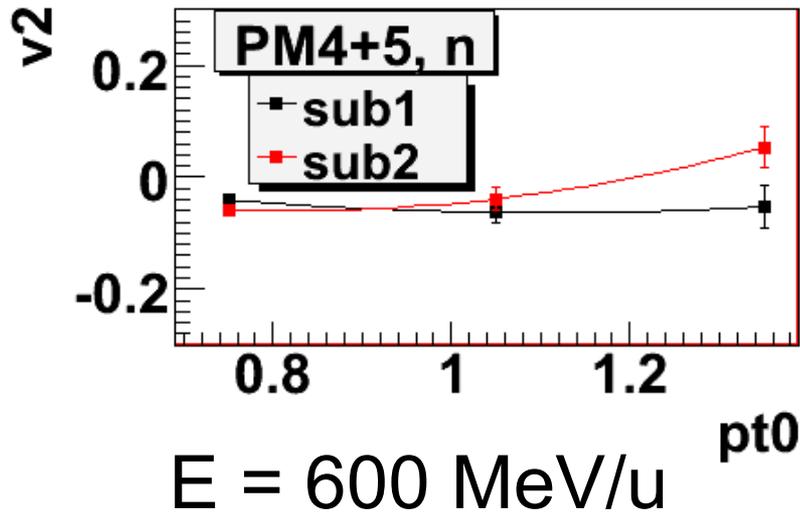
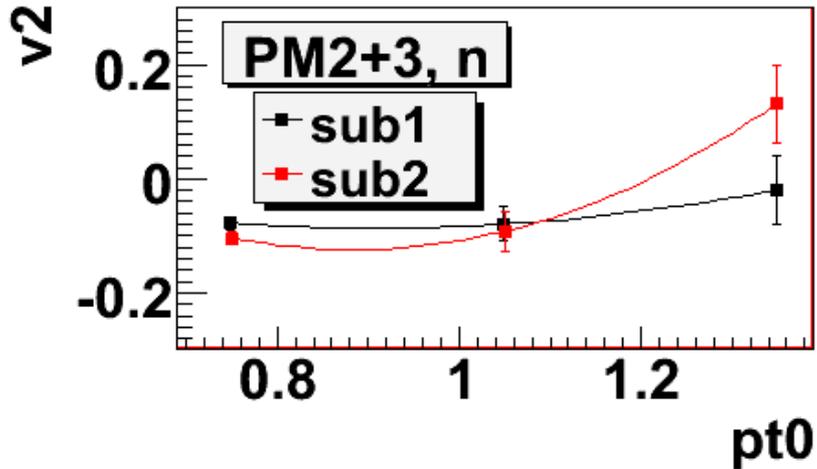
# Consistency checks

600 MeV/u

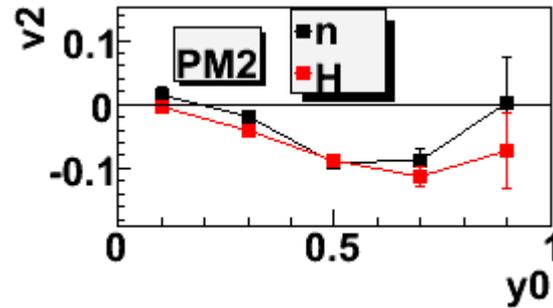
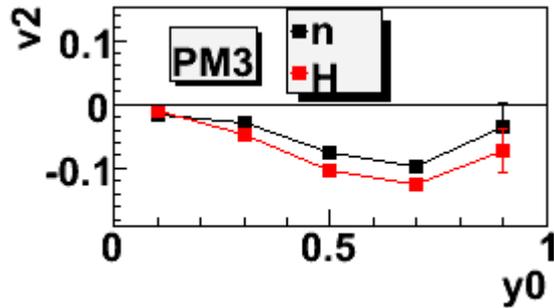


- The symmetry in  $v_2$  observable was checked for two symmetric windows in detector acceptance, for  $y_0$  and  $pt_0$ -dependence (in the next slide!)

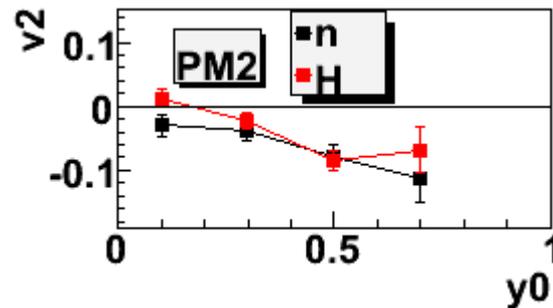
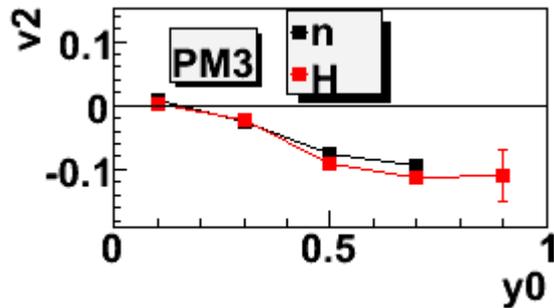
# Consistency checks



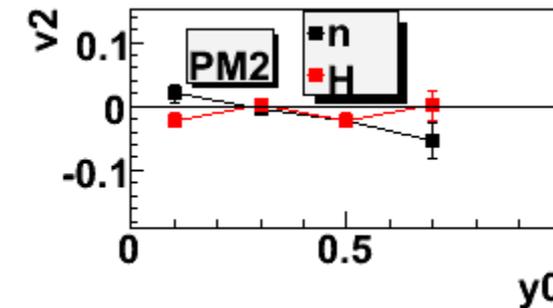
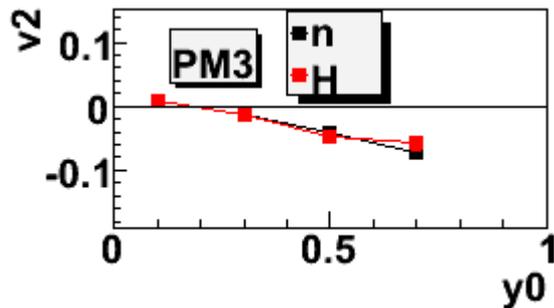
# pt integrated v2: a comparison between n and H



400 MeV/u

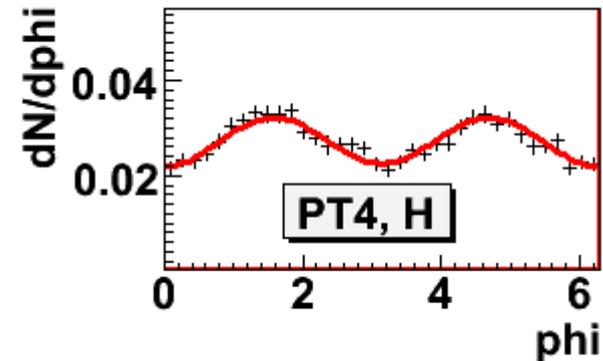
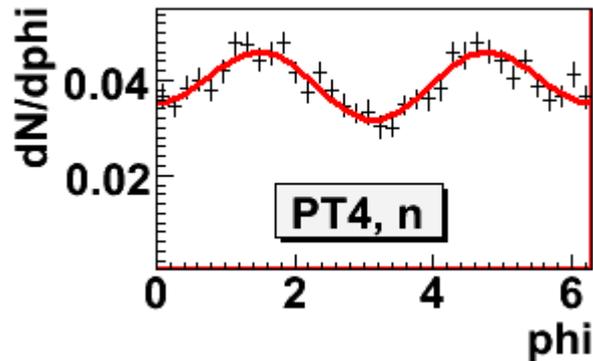
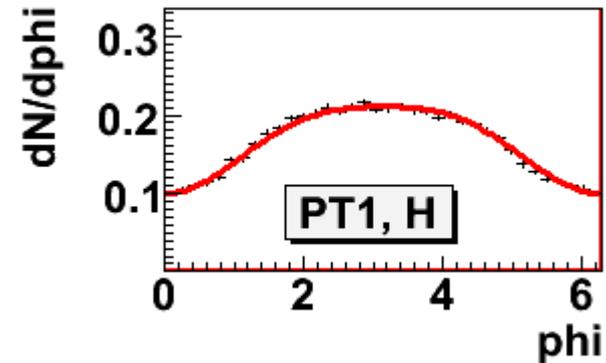
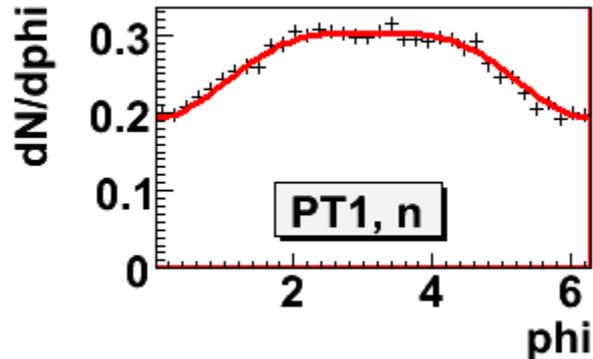


600 MeV/u



800 MeV/u

# Azimuthal distributions for PT bins



$E = 400 \text{ MeV/u}$ , central events (PM3+PM4+PM5)

$$F(\Delta\phi) = N(1 + 2(v_1\cos(\Delta\phi) + v_2\cos(2\Delta\phi)))$$

# Squeeze-out ratio definition

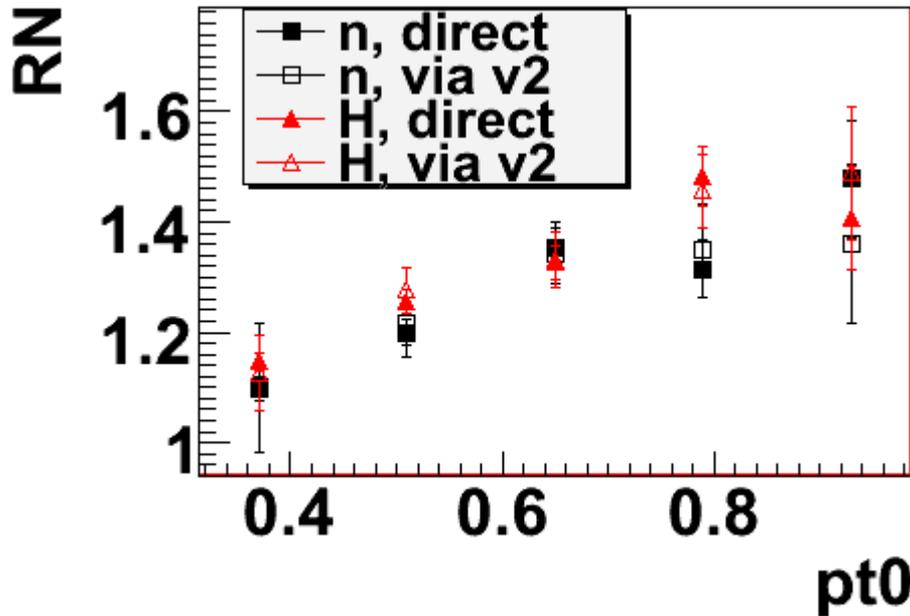
Two alternative definitions of squeeze-out ratio

$$R_N = \frac{N(90^\circ) + N(270^\circ)}{N(0^\circ) + N(180^\circ)}$$

$$R_N = \frac{1 - 2v_2}{1 + 2v_2}$$

- Squeeze-out ratio observable chosen because it exhibits stable trend in pt0-dependence
- Number of particles corresponding to the particular angle integrated within the finite range
- The integration range was varied to test the stability of result

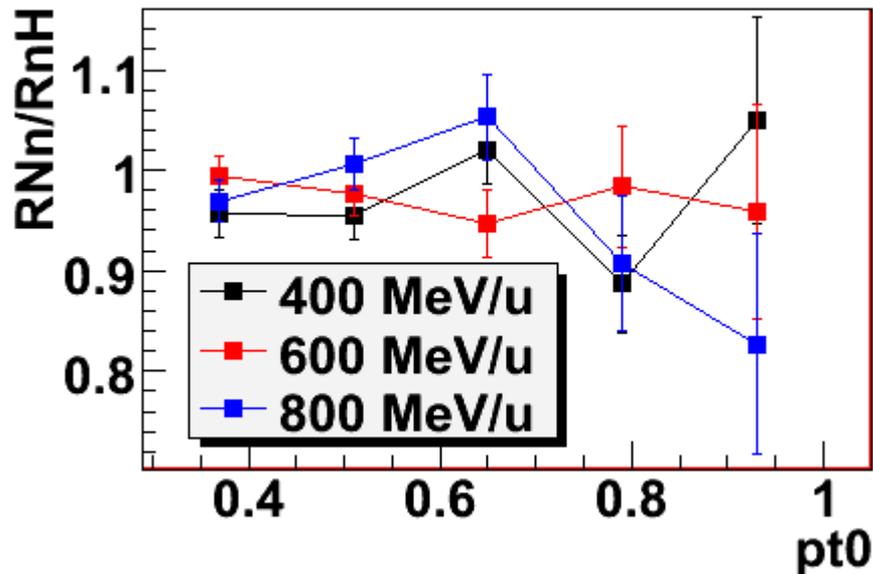
# Comparison between the two methods



- Integration range chosen to be  $\pm 10^\circ$  for 400 and 600 MeV/u, and  $\pm 6.7^\circ$  for 800 MeV/u, yielding the best agreement between two methods

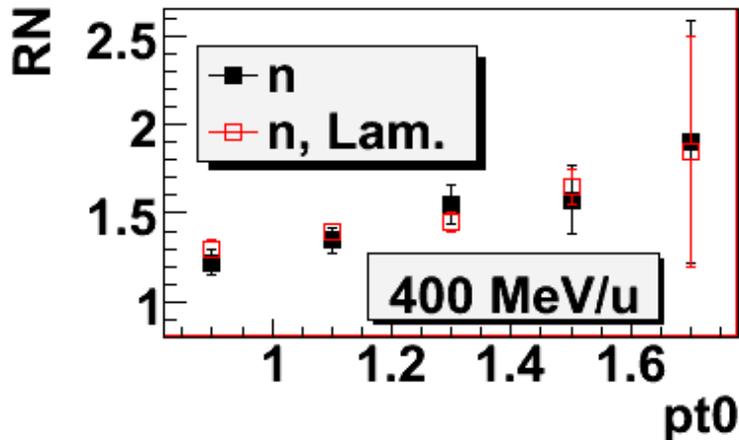
- A comparison between two methods of obtaining  $R_N$  shows satisfactory agreement. The results are shown for 400 MeV/u

# Energy and isospin dependence of differential squeeze-out ratio

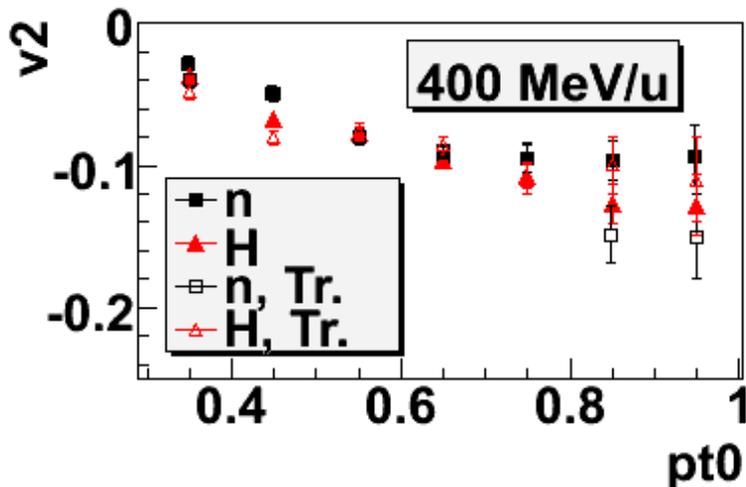


- Ratio of squeeze-out ratios is more stable with change of an integration range than the squeeze-out ratio itself
- High energy data more stable with the change of integration range

# Comparison to the previous analyses



- A comparison to D.Lambrecht paper Z. Phys. A 350 (1994) on momentum dependence shows satisfactory agreement



- The results of W.Trautmann analysis arXiv: 0907.2822 confirmed (at 400 MeV/u)

# Conclusions

- Present analysis confirms previous results on differential elliptic flow
- A shift in  $v_1$ - $y_0$  dependence becomes smaller after applied correction on reaction plane asymmetry distribution
- The squeeze-out ratio could show isospin sensitivity of elliptic flow

## Future prospects

- UrQMD simulations on squeeze out ratio dependencies as function of beam energy
- Extension of present analysis to protons
- Detailed calculation of reaction plane resolution

I would like to thank Dr. Y. Leifels from GSI, Darmstadt, for a valuable guidance during the course of the analysis and Dr. Z. Basrak from IRB, Zagreb for an important discussions. Also I would like to thank Peter Z. Wu for providing the software basis for this analysis.

Thank you for your attention!